

# Evaluation of historic Columbia River floods with HEC-RAS

Haley Dillon and Charles Cannon  
GEOG 593 – Digital Terrain Analysis  
Fall 2010

## Historic floods

Flood of 1894



City of Portland Archives

Looking north from 1<sup>st</sup> Ave. to Stark

Flood of 1948



National Weather Service; NOAA

Aerial view of the city of Vanport



City of Portland Archives

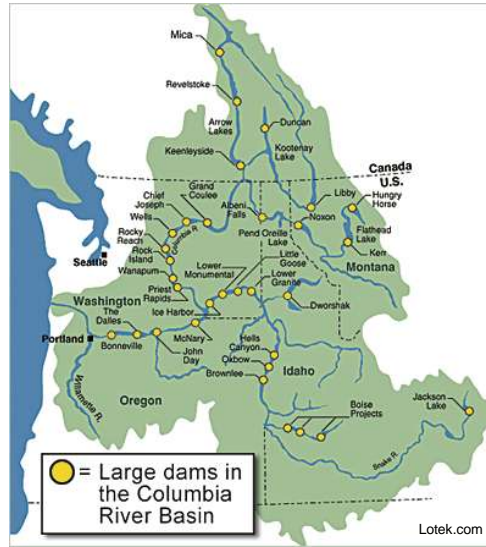
North Park Blocks looking north to Ankeny



USACE

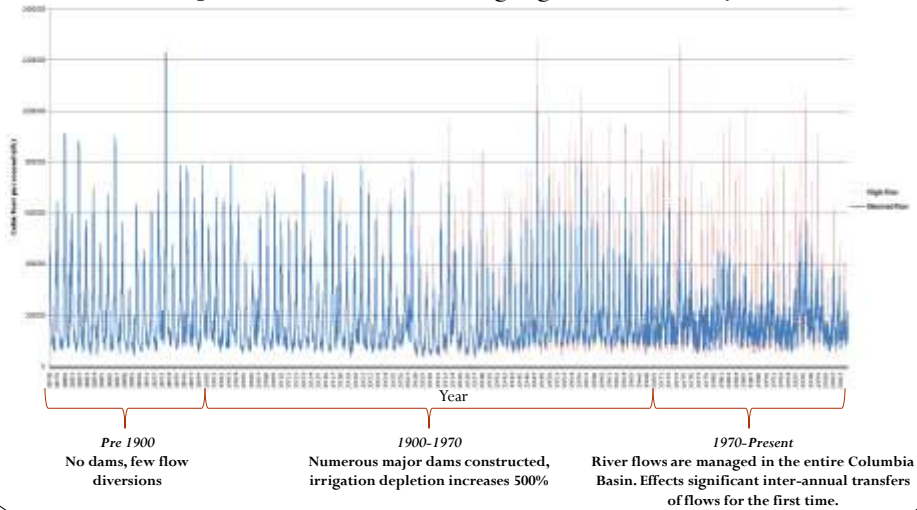
Railroad dike breach

# Altered Hydrology



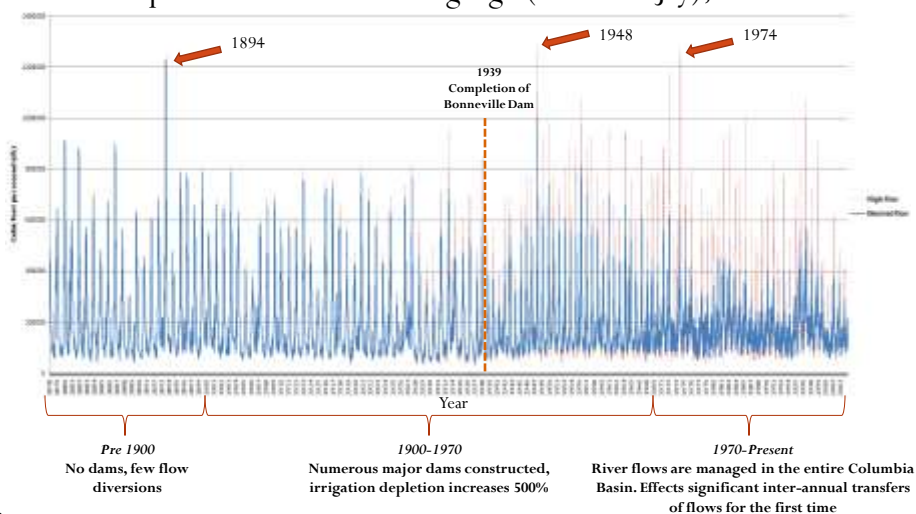
# Altered hydrology

Flood profile from The Dalles gauge (Naik and Jay), 1878-



## Altered hydrology

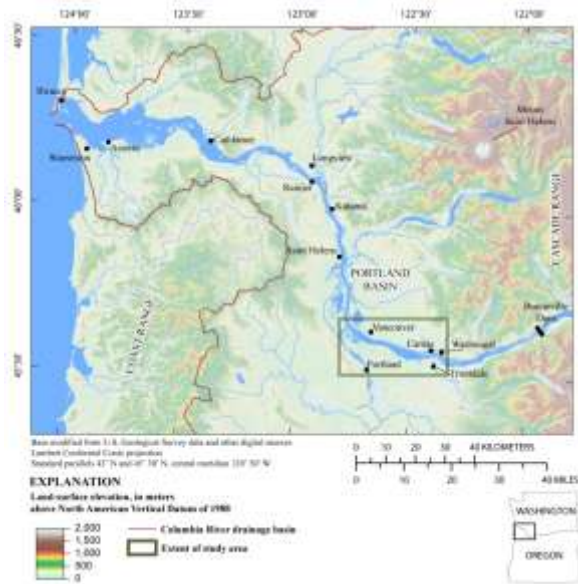
Flood profile from The Dalles gauge (Naik and Jay), 1878-2004



## Introduction

- Explanation of floodplain evolution
  - Natural floodplains are dynamic systems
  - The Columbia River flow regime has been severely altered by flow regulation, water withdrawals and probably climate change
- Habitat
  - The dynamic nature of floodplains enhances habitat through reworking of landforms during seasonal floods
  - Isolation from seasonal flows impedes landform evolution and thus decreases ecosystem function
- Safety/Economics
  - Thousands of people live and work within the Columbia River floodplain
- In this project we investigate the effects of flow regime and flood control on the area of inundated land for historic flood scenarios

## Study Area



## Methods

## HEC-RAS and HEC GeoRAS

(Hydraulic Engineering Centers River Analysis system)

- One dimensional hydraulic modeling
- HEC-RAS – developed by the US Army Corps of Engineers
- HEC-GeoRAS – allows for preparation of data for input into HEC-RAS
- Basics HEC-RAS
  - Required data – only required data is terrain data. Land use data is optional.

Required Inputs	Optional Inputs
<ul style="list-style-type: none"> <li>•Stream centerline</li> <li>•Flow path centerline</li> <li>•3D Cross sections</li> </ul>	<ul style="list-style-type: none"> <li>•Banks</li> <li>•Bridges &amp; culverts</li> <li>•Ineffective flow areas</li> <li>•Block obstructions</li> <li>•Land use</li> <li>•Levee Alignment</li> <li>•Levee points</li> <li>•Inline structures</li> <li>•Lateral structures</li> <li>•Storage areas</li> <li>•Storage area connections</li> </ul>

## Data and Preprocessing

## Source dataset

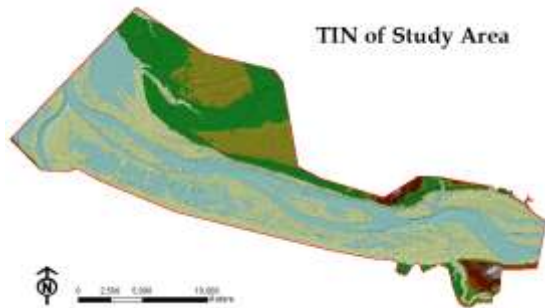
DTM	GAP Landcover
<ul style="list-style-type: none"> <li>•Data Source: Army Corps of Engineers</li> <li>•Merge of 2010 LiDAR and Bathymetry data delivered as a raster DTM. 1 meter resolution.</li> <li>•Disclaimer: data is preliminary and still in post-processing stages, scheduled to be released at a later date</li> </ul> <div style="display: flex; justify-content: space-around; align-items: center;"> <div data-bbox="317 531 642 718"> <p style="text-align: center; font-size: small;">Study Area DTM Army Corps of Engineers and USACE</p> </div> <div data-bbox="268 718 525 873"> </div> <div data-bbox="539 730 706 850" style="text-align: center;"> <p>3D view of the floodplain looking downstream from the Columbia Gorge</p> </div> </div>	<ul style="list-style-type: none"> <li>•Data Source: National Landcover Gap Analysis Project, 2010</li> <li>•Classified from remote sensing (LandSat) and elevation data</li> </ul> <div data-bbox="745 564 1142 795" style="text-align: center;"> <p style="text-align: center; font-size: small;">GAP Landcover data</p> </div>

## Pre-processing

- TIN (using ARC GIS)
- Geometry data (using HEC-GeoRAS)
  - Flow paths
  - Banks
  - 3D cross sections
  - Levee alignment table
  - Manning's N table

## TIN

- Creation:
  - Using DTM dataset
    - Tolerance of 2 m
  - Holes in original DTM were filled



## Creating Geometry Data

Flow Paths	Banks	3D Cross Sections
<ul style="list-style-type: none"> <li>•Center line</li> <li>•Left and right of channel</li> </ul>	<ul style="list-style-type: none"> <li>•Edge of channel</li> <li>•Transition from channelized to overbank flow</li> <li>•Generally drawn as inflection point in profile curvature</li> </ul>	<ul style="list-style-type: none"> <li>•Perpendicular to centerline</li> <li>•Direction is from left to right</li> <li>•Adjustment of centerline to avoid overlap</li> <li>•Must span entire floodplain</li> <li>•Attributes are               <ul style="list-style-type: none"> <li>✓River/reach</li> <li>✓Stationing (distance to downstream end of centerline)</li> <li>✓Bank stations ( )</li> <li>✓Downstream reach lengths</li> </ul> </li> <li>•2D to 3D</li> </ul>

**EXPLANATION**

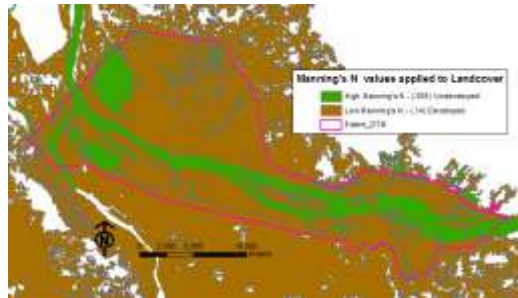
— Flow paths

— Banks

— 3D cross section cut lines

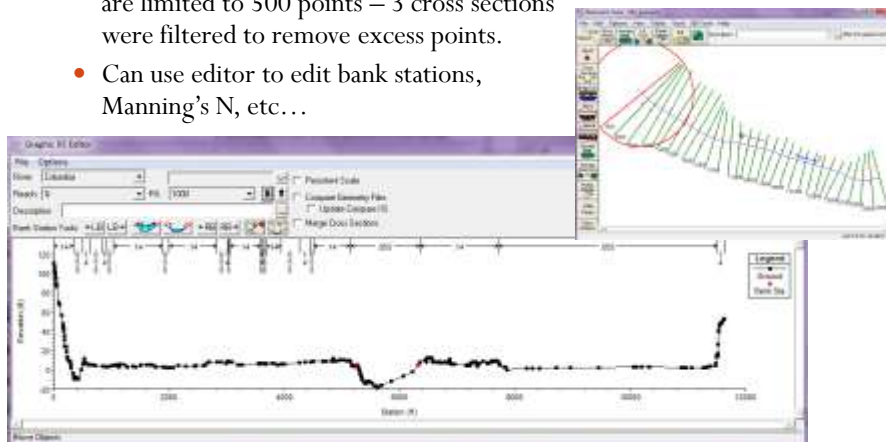
## Manning's-n

- Roughness coefficient
- Applied to land-cover dataset
- Limit of 20 per cross section in HEC-RAS
- Level 1 still too many at most cross sections
- Split into 2 groups split at 0.07
- Average assigned each group
- For three remaining cross sections with excess n-values, values were removed from right bank (Washington side)



## Importing Geometry Data into HEC-RAS

- Export to HEC-RAS format
- HEC-RAS - Edit geometry: Cross sections are limited to 500 points – 3 cross sections were filtered to remove excess points.
- Can use editor to edit bank stations, Manning's N, etc...





## Flow data and boundary conditions

- Steady flow
- Flow conditions
  - We used discharge at The Dalles gage for observed and virgin flows (estimated by Naik and Jay, 2005)
  - We developed a stage-discharge relationship for model boundary conditions which are the stage at Washougal and the Willamette River.
- Profiles used in analysis:

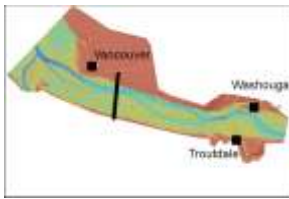
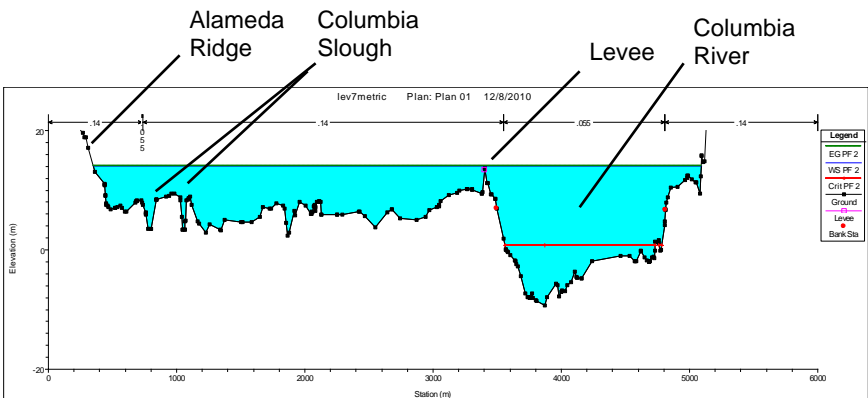


Flood Scenario	Mean Daily Discharge at The Dalles ( $\text{m}^3 \text{s}^{-1}$ )	Stage at Washougal (m, NAVD 88)	Stage at Willamette River Confluence (m, NAVD 88)
June 6, 1894 - Observed	34,830	14.0	11.6
May 30, 1948 - Observed	26,732	12.2	10.1
May 30, 1948 - Virgin	36,002	14.2	11.8
June 19, 1974 - Observed	16,084	10.0	8.0
June 19, 1974 - Virgin	35,710	14.2	11.8

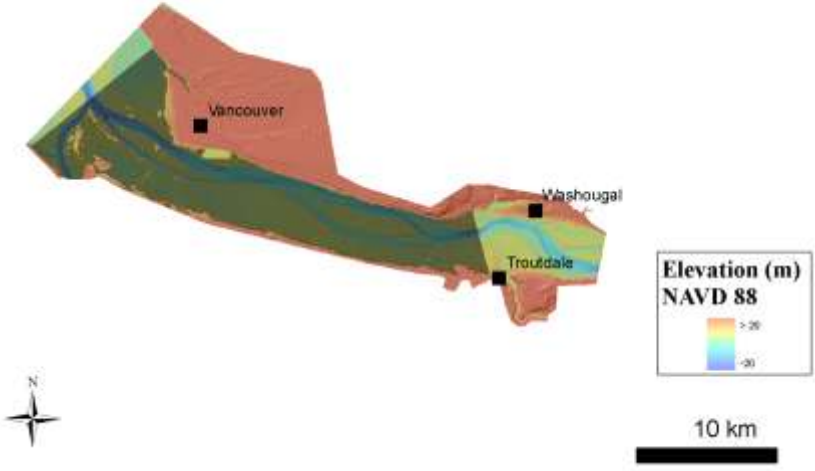
## Post-Processing

- Export the water surface profile from HEC-RAS to HEC-GeoRAS
- Convert the surface profile to a raster
- Subtract the DTM from the water surface to get inundation water depth
- The extent of the depth is the inundation area which is converted to a polygon

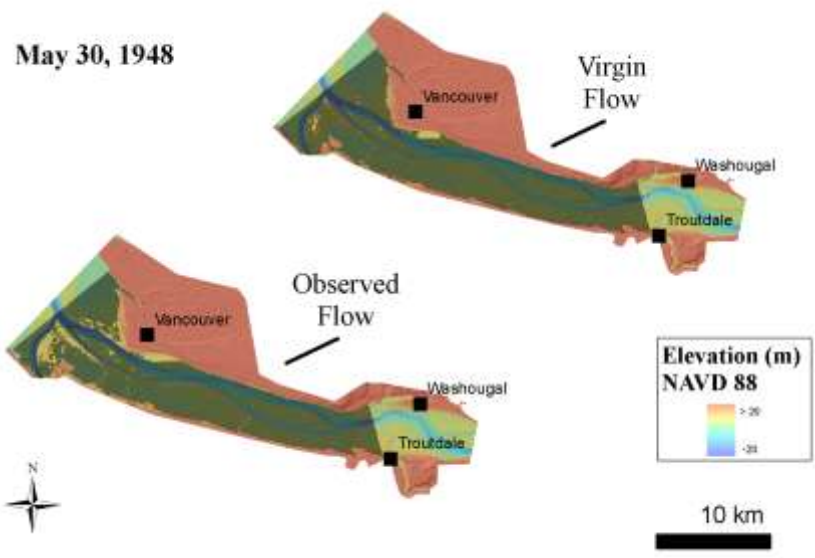
# Results

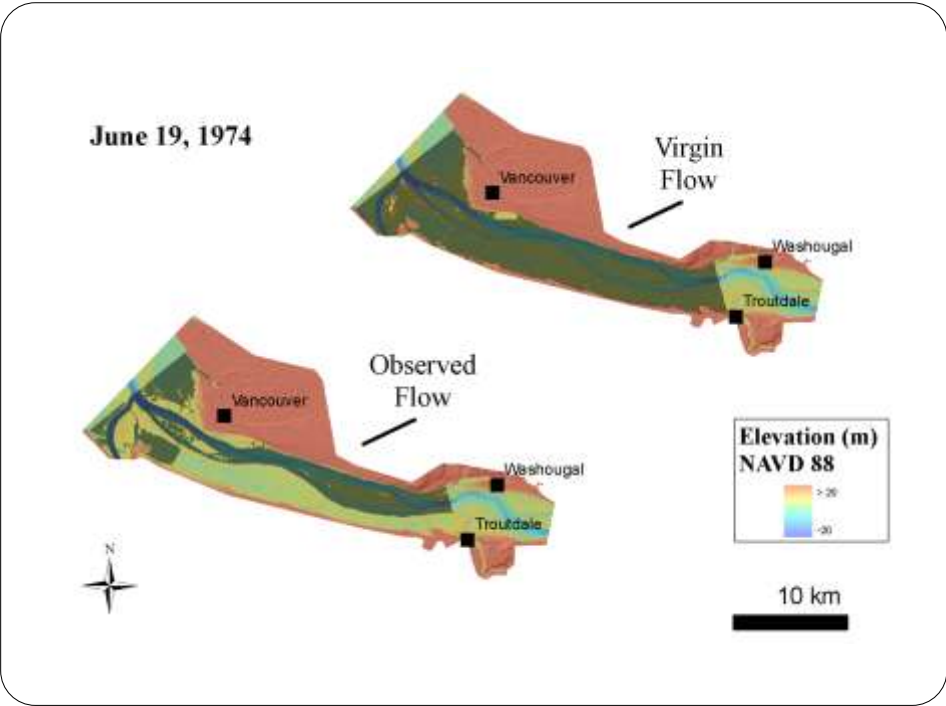


**Observed flow, June 6, 1894**



**May 30, 1948**





## Results Summary

Flood Scenario	Mean Daily Discharge at The Dalles ( $m^3 s^{-1}$ )	Stage at Washougal (m, NAVD 88)	Stage at Willamette River Confluence (m, NAVD 88)	Area ( $km^2$ )
June 6, 1894 - Observed	34,830	14.0	11.6	155,1849
May 30, 1948 - Observed	26,732	12.2	10.1	144,9921
May 30, 1948 - Virgin	36,002	14.2	11.8	156,1186
June 19, 1974 - Observed	16,084	10.0	8.0	81,7423
June 19, 1974 - Virgin	35,710	14.2	11.8	156,1081

## Conclusions



- Virgin flows for each modeled year were very similar (within 1 square kilometer)
- By the 1948 flood, large dams were being constructed system wide and irrigation depletion was increasing rapidly. A slight decrease in area (11 square kilometers) is observed and may be attributable to these factors.
- The virgin 1974 flow was discovered while processing data from The Dalles. Our HEC-GeoRAS analysis shows that if there were no alterations of the hydrology at this point in time, there could have been a flood as devastating as the largest flood on record.
- Our modeling supports the hypothesis that the modified flow regime has significantly reduced the potential for the historic Columbia River floodplain to be inundated.

## Limitations / future improvements

- Create a better Manning's N coverage
- Use a published dataset with a more complete coverage
- Add effect of tributaries
- Extend to other reaches
- Spatial resolution of modeling results
- Ground truthing

## References

- Ayres Associates, 2007, Summary of Work Performed by Ayres Associates in Support of URS Storm Surge Modeling for FEMA Region 4: retrieved online November 26, 2010 from [http://www.fema.gov/library/file?type=publishedFile&file=summary\\_of\\_work\\_performed\\_in\\_support\\_of\\_storm\\_surge\\_modeling.pdf&fileid=7198e050-e9aa-11de-ae85-001cc456982e](http://www.fema.gov/library/file?type=publishedFile&file=summary_of_work_performed_in_support_of_storm_surge_modeling.pdf&fileid=7198e050-e9aa-11de-ae85-001cc456982e)
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